		CENTRAL INTELLIGENC	E AGENCY	REPORT	
	UN	FORMATION	REPUKI		
COUNTRY	USSR			DATE DISTR. Q JULY	52
SUBJECT		Guided Missile D	evelopment	NO OF PAGES 5	25 X 1
PLACE	<u> </u>		· · · · · · · · · · · · · · · · · · ·	NO. OF ENCLS.	
ACQUIRED					
DATE ACQUIRED				SUPPLEMENT TO REPORT NO.	
DATE OF				25)	(1
OF THE UNITED STA	NTAINS INFORMATION AFFECTING THE RTES, BITHIN THE MEANING OF TITLE U.S. CODE, AS AMENDED. ITS TRAN NTENTS TO OR RECEIPT BY AN UNAUT F. THE REPRODUCTION OF THIS FOR	SMISSION OR REVE- Horized Person 1s	THIS IS UNE	VALUATED INFORMATION	
		<u> </u>		* 1	
Ap	pendix ¹ B°				
		es - See separate sh	eets attached.	25X	1
		SECRET		25X	1
		SECRET SECURITY INFORMATIO) N	25X	1
		SECRET SECURITY INFORMATIO	ION IN	25X X M/PR X ATIO	1 I
Appeview completed. WIST STATE 51-4F	Guided Missile	SECRET SECURITY INFORMATION DISTRIBUT	ION IN	25X CXM/RRXATIO X FBIX	1

25X1



(a)

(b)

(c)

<u>(d)</u>

(e)

(£)

Model

25 ton

35 ton

100 ton

Model

35

ton

is expected.

are anticipated and

realizable.

SECURITY INFORMATION 25X1 SECRET -3-Appendix 'B' Page 1 GUIDED MISSILES 25X1 expansion ratio (exit area to throat area) of the engine 25X1 Exp. Ratio Comb. Press. Theoretical Exhaust Velocity 2000 m/sec. 15 atm. 2000 m/sec. 20 atm. 16.0 60 atm. 2360 m/sec. The higher expansion ratio for the 100 ton model follows from the greater combustion pressure employed. 25X1 Max. Diam. Throat a Exit Comb. Chamber Diameter Diameter 400 mm. 740 mm. 950 " 400 740 mm. 1200 470 1800 The above are inside dimensions. The outside diameter would exceed the above by twice the depth of the cooling jacket, i.e. by about 30-50 mm. 25X1 The standard A-4 has a specific thrust of 210 Kg. If this figure is maintained for the larger (100 ton) model, the designed fuel consumption of 500 Kg/sec. would yield 105 tons thrust. With the paraffin ruel, a higher specific thrust 25X1 25X1 The theoretical value for paraffin is 240 kg., giving a maximum theoretical thrust of 120 tons for a fuel consumption of 500 Kg/sec. 25X1 The paraffin has the characteristics of ordinary Kerosene (lamp oil). The specific impulse is 240 Kg. The single stage centrifugal pumps work against a head of about 2300 ft. Pumps of known design can provide about 600-800 ft. head at high flow. It is admitted that the fuel pump (alcohol) on the standard A-4 has a delivery pressure of 25 atmospheres (800 ft.) at 3800 rpm. The same pump on the 35 ton model running at 5000 rpm., reaches a pressure of

25X1

with minor alter-

SECRET SECURITY INFORMATION

35 atmospheres (1100 ft.). These are test figures for single stage, single entry centrifugal pumps. With double entry pumps higher delivery

ations in blade design the 70 atmosphere delivery pressure should be

	SECRET		
		Appendix Page 2	'B'
(h)			
			2
- [The nozzle shape was based on theoretical considerations.		
<u>(i)</u>	Calculations show that a Hydrocarbon such as "paraffin" may be successfully to regeneratively cool an engine of this size.	used	
	The possibility of ultimately using the cooling jacket as a st generator to assist the peroxide plant was considered.	eam	
<u>(i)</u>			
	Mha and what dishaukian was to managed to the section and subscars	lom# Tax	:
	The original intention was to vapourize the water, and subseque condense it by means of liquid oxygen.	CH of A	
(<u>k)</u>			
	To the final degical the rectangue and through every		
	In the final design, the water was not thrown away.	1	
· 7 \			
(1)			
(1)			9
<u>(1)</u>			2
J			2
J	several cooling alternatives were investigated		. 2
<u>(1)</u>	several cooling alternatives were investigated it is quite possible that in the final version alcohol will		2
J	it is quite possible that in the final version alcohol will replace the paraffin, and the normal A-4 cooling process will be adopted.		2
J	it is quite possible that in the final version alcohol will replace the paraffin, and the normal A-4 cooling process		2
	it is quite possible that in the final version alcohol will replace the paraffin, and the normal A-4 cooling process will be adopted.		2
	it is quite possible that in the final version alcohol will replace the paraffin, and the normal A-4 cooling process will be adopted. The water pump is reportedly "carried" by the paraffin pump. The pumps are mounted on either side of the steam turbine, with Oxygen and Peroxide pumps on the left and the paraffin and wat pumps on the right. The casings of the individual pumps are 1	er ocated	
	it is quite possible that in the final version alcohol will replace the paraffin, and the normal A-4 cooling process will be adopted. The water pump is reportedly "carried" by the paraffin pump. The pumps are mounted on either side of the steam turbine, wit Oxygen and Peroxide pumps on the left and the paraffin and wat	er ocated	2
	it is quite possible that in the final version alcohol will replace the paraffin, and the normal A-4 cooling process will be adopted. The water pump is reportedly "carried" by the paraffin pump. The pumps are mounted on either side of the steam turbine, wit Oxygen and Peroxide pumps on the left and the paraffin and wat pumps on the right. The casings of the individual pumps are 1 on each other, by means of special pads and the drive is by a	er ocated common	
(m)	it is quite possible that in the final version alcohol will replace the paraffin, and the normal A-4 cooling process will be adopted. The water pump is reportedly "carried" by the paraffin pump. The pumps are mounted on either side of the steam turbine, with Oxygen and Peroxide pumps on the left and the paraffin and wat pumps on the right. The casings of the individual pumps are 1 on each other, by means of special pads and the drive is by a sub-divided shaft. For the flow rate of Hydrogen Peroxide, the calculated turbine	er ocated common	
(m)	it is quite possible that in the final version alcohol will replace the paraffin, and the normal A-4 cooling process will be adopted. The water pump is reportedly "carried" by the paraffin pump. The pumps are mounted on either side of the steam turbine, wit Oxygen and Peroxide pumps on the left and the paraffin and wat pumps on the right. The casings of the individual pumps are 1 on each other, by means of special pads and the drive is by a sub-divided shaft. For the flow rate of Hydrogen Peroxide, the calculated turbine efficiency is 55%.	er ocated common	
(m)	it is quite possible that in the final version alcohol will replace the paraffin, and the normal A-4 cooling process will be adopted. The water pump is reportedly "carried" by the paraffin pump. The pumps are mounted on either side of the steam turbine, wit Oxygen and Peroxide pumps on the left and the paraffin and wat pumps on the right. The casings of the individual pumps are 1 on each other, by means of special pads and the drive is by a sub-divided shaft. For the flow rate of Hydrogen Peroxide, the calculated turbine efficiency is 55%.	er ocated common	

SECRET SECURITY INFORMATION

	SECRET	1	
	SECURITY INFO	DRMATION [2
3	- 5	-	Appendix 'B'
			Page 3
	The weight of the 100 tons combustion is 800 Kg. The turbo-pump unit consirotor diameter) together with:-	chamber together with the sts of the 2-stage steam t	Orthones was -
	Oxygen pump	320 mm rotor	
	Paraffin " ceeege	360 mm rotor	
	Water "	210 mm rotor	
	Peroxide "	280 mm rotor	
	The estimated design weight of the co 350 Kg. Other component weights not	mplete 2—stage steam turbi known•	ne assembly is
e:	The turbo-pump assembly of the standar	rd V.2 weights 180 Kg?	
i			2
(p)	'		· · · · · · · · · · · · · · · · · · ·
			:
ŗ	The liner consisted of pure copper (continuous is 1 mm at the bridge pieces outer steel shell is 5 mm thick, and	B with 1 mm at the coldonor	ion (1) the
(p)		1	2
(4)	'		
			2
1			
(r)	In the second chamber design, a second	l flat copper sheet was wel	ded to the inner
(r)	In the second chamber design, a second side of the corrugated conner plate	l flat copper sheet was wel	ded to the inner
(r)	In the second chamber design, a second side of the corrugated conner plate	l flat copper sheet was wel	ded to the innor
(r)	In the second chamber design, a second side of the corrugated corresponds	l flat copper sheet was wel	ded to the innor
(r)	In the second chamber design, a second side of the corrugated conner plate	l flat copper sheet was wel	ded to the inner
(r)	In the second chamber design, a second side of the corrugated conner plate.	l flat copper sheet was wel	ded to the inner
(r)	In the second chamber design, a second side of the corrugated conner plate	l flat copper sheet was wel	ded to the inner
(r)	In the second chamber design, a second side of the corrugated conner plate	l flat copper sheet was wel	ded to the inner
(r)	In the second chamber design, a second side of the corrugated conner plate	l flat copper sheet was wel	ded to the inner
(r)	In the second chamber design, a second side of the corrugated conner plate	l flat copper sheet was wel	ded to the inner
(r)	In the second chamber design, a second side of the corrugated conner plate.	l flat copper sheet was wel	ded to the inner
(r)	In the second chamber design, a second side of the corrugated conner plate.	l flat copper sheet was wel	ded to the inner
(r)	In the second chamber design, a second side of the corrugated conner plate.	l flat copper sheet was wel	ded to the inner
(r)	In the second chamber design, a second side of the corrugated conner plate.	l flat copper sheet was wel	ded to the inner
(r)	In the second chamber design, a second side of the corrugated conner plate.	l flat copper sheet was wel	ded to the innon
(r)	In the second chamber design, a second side of the corrugated conner plate.	l flat copper sheet was wel	ded to the inner
(r)	In the second chamber design, a second side of the corrugated conner plate.	l flat copper sheet was wel	ded to the inner
(r)	In the second chamber design, a second side of the corrugated conner plate	l flat copper sheet was wel	ded to the inner
(r)	In the second chamber design, a second side of the corrugated conner plate.		
(r)	In the second chamber design, a second side of the corrugated conner plate.	a thrust frame	

end -

SECRET SECURITY INFORMATION